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### FUEL CELL ASSEMBLY

The present invention relates to fuel cells and is particularly concerned with a tubular solid oxide fuel cell assembly.

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Fuel cells convert gaseous fuels (such as hydrogen, natural gas, and gasified coal) directly into electricity via an electrochemical process. A fuel cell continuously produces power when supplied with fuel and oxidant, normally air or other oxygen-containing gas. A typical fuel cell consists of an electrolyte (ionic conductor,  $H^+$ ,  $O^{2-}$ ,  $CO_3^{2-}$ , etc.) in contact with two electrodes (mainly electronic conductors). On shorting the cell through an external load, fuel oxidises at the anode resulting in the release of electrons which flow through the external load and reduce oxygen at the cathode. The charge flow in the external circuit is balanced by ionic current flows within the electrolyte. At the cathode oxygen from the air or other oxidant is disassociated and converted to oxygen ions which migrate through the electrolyte membrane and react with the fuel at the anode/electrolyte interface. The voltage from a single cell under typical load conditions is in the vicinity of 0.6 to 1.0V DC and current densities in the range of 100 to 1000  $mAcm^{-2}$  can be achieved.

Several different types of fuel cells are under development. Amongst these, the solid oxide fuel cell (SOFC) is regarded as potentially the most efficient and versatile power generation system, in particular for dispersed power generation, with low pollution, high efficiency, high power density and fuel flexibility.

Numerous SOFC configurations are under development, including the planar, the tubular, the segmented and the monolithic designs. The planar or flat plate design has been widely investigated. In this concept, the components - electrolyte/electrode laminates and interconnect or gas separator plates, which may have gas channels formed therein - are fabricated individually and then stacked together and sealed with a high temperature sealing material to form either a fixed or sliding seal.

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SOFCS operate in the vicinity of 700 - 1000°C, and planar SOFCs are inherently difficult to seal, especially as a consequence of thermal shock and cycling. Furthermore, because of the way planar SOFCs are stacked with interconnects or gas separators therebetween, the interconnects add mass and complexity of materials to the planar SOFC design.

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Many of the disadvantages of planar SOFCs are alleviated in tubular SOFCs. In the tubular concept, one of the oxygen-containing gas and fuel gas is passed along the interior of the tube, while the other gas is passed over the exterior.

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In designs proposed by Westinghouse, the oxygen-containing gas is supplied to the interior of the tubular fuel cell, so the cathode is on the inside, whereas in designs proposed by Mitsubishi the fuel gas is supplied to the interior of the tubular fuel cell, so the anode is on the inside. In both proposals, the fuel cell assemblies including the fuel cell and the current collectors on both the anode and cathode sides are formed of ceramic or cermet materials leading to a structure which is susceptible to the fragility of these inherently brittle materials. Additionally, these tubular current collectors have an inherently long electron flow path compared to those of other designs and, since the electronic conductivities of the anode and cathode materials are relatively low, resistive losses tend to be high. This feature has tended to limit the power densities of tubular fuel cells and/or has required relatively large structures to achieve the desired currents.

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Furthermore, because of the relatively poor thermal conductivity of ceramic materials, thermal or power variations within a tubular fuel cell formed primarily of ceramic materials, or within a bundle of such tubes, can cause relatively high localised temperature gradients which in turn introduce high localised strains into the tube(s). These can lead to the fracture of the tube(s).

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In International Patent Application WO 99/17390 there is proposed an SOFC tubular fuel cell assembly in which the anode is on the inside and the cathode is on the outside of the tube. On the cathode it is proposed that an electrically conducting layer formed of silver wire or silver paste be provided. The electrons produced at the anode are passed to a current collector made of nickel and consisting of a number of wires twisted around each other.

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According to a first aspect of the present invention there is provided a tubular fuel cell assembly comprising an anode side defining a passage for fuel gas, the anode side comprising an anode layer and an anode-side current collector in electrical contact with the anode layer, a solid oxide electrolyte layer on a radially outer surface of the anode layer, a cathode layer on a radially outer surface of the electrolyte layer, and a cathode-side current collector on the cathode layer, wherein the anode-side current collector comprises a tubular metallic structure which is adapted to permit fuel gas in the passage to contact the anode layer, at least the surface of the tubular metallic structure being formed of Ni or Ni alloy, and wherein the tubular metallic structure is at least partly embedded in the anode layer.

By the first aspect of the present invention, the current collection on the anode side of the fuel cell is substantially improved over nickel cermet current collectors, with an electrical conductivity about 500 times greater at the operating temperature of an SOFC, about 700 to 1000°C, and a greatly improved thermal conductivity. This permits substantially smaller devices to be adopted and losses to be reduced. Additionally, by at least partly embedding the tubular metallic structure of the anode side current collector in the anode layer, the tubular metallic structure provides a degree of reinforcement to the SOFC, also permitting smaller devices to be adopted while at the same time improving thermal and mechanical shock resistance. This may allow the fuel cells to be employed in smaller and possibly even mobile applications.

The overall diameter of the tubular fuel cell assembly may be in the range 2 to 20mm or larger, preferably 3 to 10mm. Each tubular fuel cell assembly may have any desired length, for example in the range of about 90 to 1000mm, preferably 200 to 300mm. A plurality of the tubular fuel cell assemblies may be disposed side by side or bundled together and electrically connected in parallel or in series. The tubular fuel cell assemblies should be spaced from each other to permit oxygen-containing gas, preferably air, to flow over the cathode layers.

The anode layer is preferably a nickel cermet, for example Ni/ZrO<sub>2</sub>, but other ceramic-type materials may be contemplated. The anode layer is preferably relatively thin with a thickness in the range of about 50 to 500 µm, for example about 200 µm. The anode layer is a porous layer which may be formed by any of a variety of suitable tube forming methods. Most

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advantageously, the tubular metallic structure of the anode-side current collector is at least partly embedded in the anode layer by disposing the material of the anode layer in a green condition, for example the nickel cermet in particulate form mixed with a binder, on to a previously-formed tubular metallic structure. During this process the tubular metallic structure will become at least partly embedded in the green material, optionally with the application of pressure to the green material and/or to the tubular metallic structure if this has a degree of stretch. The green material is then dried, usually by sintering. The green material may be disposed on the tubular metallic structure by, for example, casting, drawing or extruding. Preferably the anode layer is extruded. The extrusion may be performed hot, warm or cold. Drying and/or sintering of the preferred cermet material may be assisted by microwave heating.

In one embodiment, the tubular metallic structure may be at least substantially completely embedded in the anode layer, for example just having its radially inner surface exposed in the passage of the fuel cell assembly, but this is not essential to providing the degree of reinforcement to the assembly. The reinforcement may be adequately provided by a simple physical interengagement or interlocking between the anode layer and tubular metallic structure. Such interengagement could be provided by the tubular metallic structure having surface formations thereon which project radially outwardly into the anode layer, or, for example, by the tubular metallic structure having concave formations on a radially outer surface thereof into which the anode layer extends, and the term "at least partly embedded" shall be construed accordingly.

The tubular metallic structure of the anode side current collector may take any of a variety of forms, or a combination of two or more of these forms, and may have a thickness in the range of about 20 to 200 $\mu$ m or greater depending upon the configuration and, for example, the desired current density. Preferably, the tubular metallic structure extends the full length of the tubular passage.

In one embodiment, the tubular metallic structure may comprise a spiral or mesh of nickel or nickel alloy thread.

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Alternatively or in addition, the tubular metallic structure may comprise a support tube which is at least substantially rigid and is formed of or coated with nickel or nickel alloy. The support tube must permit free flow of fuel gas to the anode layer and thus it may comprise an expanded or woven mesh or otherwise perforated tube of nickel or nickel alloy. Instead, the support tube may be formed of a porous nickel material. Alternatively, the support tube may comprise a nickel or nickel alloy surface layer on a substrate of, for example, a heat resistant metal acting as the primary heat conductor for each tubular fuel cell assembly. The substrate may be an expanded or woven mesh or otherwise perforated tube with perforated nickel or nickel alloy foil wrapped over the sheet, or with nickel or nickel alloy deposited or otherwise coated onto it.

Several construction variations are possible, for example Ni mesh on steel mesh, Ni plated mesh on Ni plated steel mesh, centrifugally cast Ni spiral on Ni plated steel mesh or perforated Ni sheet wrapping on plain steel mesh, with the steel optionally being replaced by another thermally conductive material with adequate high temperature properties. As noted above, the nickel or nickel alloy layer may have a thickness in the range of about 20 to 200 $\mu$ m. The substrate may have a thickness in the range of about 0.05 to 0.5 mm.

An advantage of combining the aforementioned spiral or mesh thread current collector with the support tube is that the support tube may provide optimum electrical and thermal conductivity as well as mechanical shock resistance, while the thread current collector may be much finer in scale and provide more effective electron collection. The thread may be wound or otherwise provided on the support tube.

As an alternative to, or in addition to, an at least substantially rigid support tube which acts as a heat conductor as well as an electrical conductor, a separate tube liner may be used within the passage of the fuel cell assembly to act as a superior thermal conductor, for example of copper. The tube liner may itself be tubular or have any other suitable cross-section. A copper tube liner may have those surfaces exposed to the nickel on the anode side of the fuel cell protected with, for example, alumina to prevent poisoning of the nickel when the nickel is to be used as a catalyst for steam reforming of methane fuel gas supplied to the passage.

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To allow for the differential expansion of the tube liner during thermal cycling of the tubular fuel cell assembly, and for ease of assembly, the tube liner may be a loose fit in the passage of the tubular fuel cell assembly at least at room temperature and expand into contact with the anode-side current collector at the operating temperature of the fuel cell assembly.

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Alternatively the anode layer may be extruded alone to an internal diameter such that, after drying, the tubular metallic structure may be easily slipped inside the anode layer. However before its insertion, the tubular metallic structure may be coated in a cermet slurry on its outside and dried in order to ensure the at least partial embedding of the tubular metallic structure in the anode layer.

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Commercially pure nickel is preferred for the anode-side current collector, or at least the surface thereof. This is available as, for example, alloy types 200 and 201 from Inco Alloys International. The nickel alloy which may be provided at at least the surface of the tubular metallic structure should contain Ni as the major component, preferably at a level greater than 50% by weight, and the other alloying element or elements should not be detrimental to the performance of the tubular fuel cell assembly. Copper-free nickel alloys are preferred in order to provide CH<sub>4</sub> reforming capability at the anode side of the fuel cell assembly. Chromium-free alloys are also preferred to avoid Cr contamination of the cathode side and consequent total failure of the or each fuel cell assembly in the event of leakage of Cr from the anode side. Other properties required of a suitable nickel alloy include high electrical conductivity, low creep at the operating temperatures, no reaction with the fuel gases (except to catalyse CH<sub>4</sub> reforming if desired), and low levels of "dusting" disintegration.

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The solid oxide electrolyte layer is preferably a Y<sub>2</sub>O<sub>3</sub> doped ZrO<sub>2</sub>, for example 8YSZ. Preferably the solid oxide electrolyte layer is relatively thin with a thickness less than 70 μm, for example about 20 μm or less. The electrolyte is preferably continuous along the full length and around the circumference of the tubular anode layer and may be formed in any of a variety of ways bearing in mind that the electrolyte layer must be a dense, defect-free layer to prevent mixing of the fuel gas and oxygen-containing gas through the fuel cell. The electrolyte material may be deposited onto the tube by, for example, slurry coating. Other possible methods include

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extrusion onto the anode layer or co-extrusion with it, sol gel spin casting and electrophoretic coating.

A variety of different materials are known for use as the cathode layer of a solid oxide fuel cell, but the currently preferred materials are perovskites such as strontium doped lanthanum manganite (LSM) and/or strontium doped praseodymium manganite (PSM) or La cobaltites, preferably having a total thickness in the range of about 30 to 100  $\mu\text{m}$ . The cathode layer may be applied by, for example, slurry spraying or any other form of slurry coating, screen printing or extrusion.

In a preferred embodiment, the cathode layer is discontinuous along the tubular fuel cell assembly to provide a plurality of longitudinally spaced cathode portions. This effectively provides a plurality of adjacent fuel cells in the tubular fuel cell assembly, albeit with a common anode layer and a common solid oxide electrolyte layer.

According to a second aspect of the present invention there is provided a tubular fuel cell assembly comprising an anode-side defining a tubular passage for fuel gas, the anode-side comprising an anode layer and an anode-side current collector in electrical contact with the anode layer, a solid oxide electrolyte layer on a radially outer surface of the anode layer, a cathode layer on a radially outer surface of the electrolyte layer, and a cathode-side current collector on the cathode layer, wherein the cathode layer is discontinuous along the length of the assembly to provide a plurality of longitudinally spaced cathode portions.

In one embodiment of a tubular fuel cell assembly including a plurality of cathode portions, the adjacent individual portions of the cathode layer are separated longitudinally by a gap in the range of about 2 to 10 mm about every 25 to 80 mm, most preferably about every 40 to 50 mm. Likewise, the cathode layer may have one or more similar gaps extending axially along the tube, preferably with two diagonally opposed gaps. The individual portions of the divided cathode layer may be electrically connected with adjacent portions along and/or around the tube, and/or with adjacent tubular fuel cell assemblies in a fuel cell bundle. This helps to maintain the performance of the tubular fuel cell assembly should the cathode side of the assembly be

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damaged.

Preferably, the cathode layer of the tubular fuel cell assembly in accordance with the second aspect of the invention is applied by, for example, extrusion slurry coating or screen printing.

- 5 The gap or gaps defining the cathode layer portions may be formed in the cathode layer as the cathode layer is applied, by any suitable technique which may be readily identified by one skilled in the art according to the technique by which the layer is applied. The cathode layer portions preferably have a thickness in the range of about 30 to 100 $\mu$ m. Currently preferred materials are perovskites such as strontium doped lanthanum manganite (LSM) and/or strontium  
10 doped praseodymium manganite (PSM) or La cobaltites.

- The anode side current collector of the tubular fuel cell assembly in accordance with the second aspect of the present invention may comprise a nickel cermet as is known from the prior art, but preferably is in accordance with the first aspect of the present invention, optionally with any of  
15 the preferred features associated therewith which for convenience only will not be described again.

- Similarly, the anode layer, solid oxide electrolyte layer, and other features of the tubular fuel cell assembly in accordance with the second aspect of the present invention are each preferably as  
20 described in accordance with the first aspect of the present invention, optionally with any of the preferred features associated therewith, and for convenience only will not be described again.

- The cathode side current collector in accordance with the first or second aspect of the invention must be adapted to permit oxygen-containing gas around the fuel cell to contact the cathode  
25 layer, and preferably comprises a metallic material having a relatively high electrical conductivity. Such a metallic current collector may comprise a mesh which is advantageously screen printed or otherwise deposited on the cathode layer, or a respective mesh preferably applied by any of these methods on each portion of the preferred divided cathode layer. Such a mesh may have a thickness in the range of about 20 to 100 $\mu$ m. Especially, but not only, where  
30 the cathode layer is divided longitudinally to form plural fuel cells along the tube, one or more electrically conductive metallic strips, which form part of the cathode-side current collector and



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may be of the same material as the mesh if same is provided, may extend the length of the tubular fuel cell assembly, or part of it, and be screen printed or otherwise deposited on the cathode layer. If a metallic strip bridges two or more of the plural fuel cells it may electrically connect them in series. Alternatively, or in addition, the individual fuel cells may be connected  
5 by other means, such as electrically conductive blocks, in series or in parallel, that is with adjacent fuel cell assemblies. The aforementioned meshes or other current collector may be deposited over the metallic strip or strips or at least one of the metallic strips, or be otherwise electrically connected thereto. The or each metallic strip could be disposed on the electrolyte layer in a respective longitudinal gap in the cathode layer, but in electrical contact with the  
10 cathode side current collector, in which case it may have a width less than the longitudinal gap. The or each metallic strip may have a thickness in the range of about 100 to 200 $\mu$ m, preferably about 100  $\mu$ m.

Preferably, the metallic material of the cathode side current collector is silver, but other noble  
15 metals, such as platinum, or their alloys would be suitable. Current collection on the cathode side of the fuel cell using a noble metal is substantially improved over the known ceramic-based current collectors, with an electrical conductivity of about  $4 \times 10^5$  S/cm for silver being >10,000 times higher at the operating temperature of an SOFC. This permits substantially smaller structures to be adopted. Additionally, the noble metal or alloy current collector may provide  
20 a degree of reinforcement to the SOFC, also permitting smaller structures to be adopted while at the same time improving shock resistance.

The shock resistance of a tubular fuel cell assembly in accordance with either aspect of the present invention may be greatly enhanced by providing a fuel cell bundle comprising a plurality  
25 of fuel cell assemblies according to the invention each mechanically connected to one or more adjacent tubular fuel cell assemblies, for example in a honeycomb structure.

The mechanical connection between the tubular fuel cell assemblies may be continuous along at least part of the length of the fuel cell assemblies or intermittent. The mechanical connection  
30 may be flexible or rigid, and it may be achieved by, for example, soldering or welding. Conveniently, the mechanical connection may also provide an electrical connection between the

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adjacent tubular fuel cell assemblies. Advantageously this may be done using the same material for the mechanical connection as the material of the cathode side current collector.

One embodiment of a tubular fuel cell assembly in accordance with the present invention will now be described by way of example only with reference to the accompanying drawings in which:

Figure 1 is a cross-section through one embodiment of a single tubular fuel cell assembly;

Figure 2 is a perspective view of a bundle of 18 of the tubular fuel cell assemblies of Figure 1, each fuel cell assembly having plural fuel cells, the fuel cells in some of the assemblies being

connected in series, but in others not, as shown in Figure 3;

Figures 3a and 3b together are a plan view of the bundle of Figure 2, partially cut away and not to scale, showing in Figure 3a the series connection of the aligned cells in each assembly and in Figure 3b the lack of series connection; and

Figures 4a and 4b together are a schematic end view of a bundle of 18 of the tubular fuel cell assemblies of Figure 1 showing two alternative means for linking adjacent fuel cell assemblies in parallel.

Referring to Figure 1 of the drawings there is shown in cross-section (not to scale) a tubular fuel cell assembly 10 comprising a porous Ni ZrO<sub>2</sub> cermet anode layer 12 defining a tubular passage 14 for fuel gas at the inner surface of the fuel cell assembly. A mesh 16 of nickel strands is partly embedded in and therefore, in electrical contact with the anode layer 12. The partial embodiment of the mesh 16 (not clearly illustrated in Figure 1) is such that the mesh is fast with the anode layer so that the mesh reinforces the cermet material of the anode layer. The mesh has a thickness of about 50µm and the spacing between strands is 1-2mm. The nickel mesh 16 is connected to electrical connectors (not shown) and acts as a current collector on the anode side. The nickel mesh 16 is preformed and the material of the porous anode layer 12 may be extruded onto it from a die and then sintered.

The porous anode layer 12 may have a thickness of about 200 µm, and a dense 8YSZ solid oxide electrolyte layer 18 having a thickness of about 20 µm is disposed continuously over the anode layer 12. The material of the electrolyte layer 18 may be co-extruded green with the

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material of the anode layer and cured, extruded green on to the anode layer and cured, or, for example, first formed by casting and rolling into a green tape which is spirally wound onto the tubular anode layer and then cured. Curing must result in a fully dense layer such that the fuel gas and oxygen-containing gas can not pass through the electrolyte layer.

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A porous cathode layer 20, for example of or incorporating LSM, having a thickness of about 50  $\mu\text{m}$  is disposed on the electrolyte layer 18 by slurry coating followed by curing.

10 The cathode layer 20 is discontinuous around the circumference of the tubular fuel cell assembly 10, with two diagonally opposed longitudinal gaps 22 defining the discontinuity. In addition, although not shown in Figures 1 and 4, the cathode layer 20 is divided longitudinally by circumferential gaps 23 such as shown in Figures 2 and 3. As with the gaps 22, the circumferential gaps 23 extend through to the electrolyte layer 18 to effectively provide a series of individual fuel cells with common electrolyte and anode layers 18 and 12 as well as a common anode side current collector 16. The overall diameter of the tubular fuel cell assembly 15 10 may be 10 mm and the gaps 22 and 23 between adjacent portions of the cathode layer 20 may be about 4 mm in width, but smaller and larger versions are possible.

20 A respective mesh 24 of silver is disposed over each portion of the cathode layer 20, each of which may be screen printed onto the cathode layer portion. The silver meshes 24 disposed over each circumferentially spaced longitudinal array of cathode layer portions may be electrically connected to each other by a respective longitudinal strip 26 of silver which may be screen printed onto the cathode layer 20 adjacent a respective one of the longitudinal gaps 22 between the cathode layer portions. Each strip 26 has a width of about 3 mm and a thickness of about 25 100 $\mu\text{m}$ . Thus, in this embodiment, the circumferentially adjacent silver meshes 24 are not connected directly, but the longitudinally adjacent silver meshes 24 are connected by the silver strips 26. Alternatively, a respective silver strip 26 is provided for each cathode layer portion. The silver strips may be regularly connected to electrical connectors (not shown) to allow for current collection when fuel gas such as moist hydrogen is passed through the tubular passage 30 14 and oxygen-containing gas such as air is passed over the cathode layer 20 at the SOFC operating temperature of 700 to 1000°C.

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Figures 2 and 3 show a bundle 38 of 18 tubular fuel cell assemblies 10 in six columns of three. Each assembly 10 in Figure 3a has two longitudinal series of silver strips 26 with each silver strip 26 associated with a respective cathode layer portion and fuel cell. Such an arrangement is also shown in Figure 2, although, for convenience only, the silver strips 26 have only been  
5 shown in the foremost column of three assemblies 10.

As shown clearly in the alternative embodiment of Figure 3b, the four fuel cells separated by three circumferential gaps 23 in the cathode layer 20 and the silver mesh 24 in each fuel cell assembly 10 are connected in series by the diagonally opposed longitudinally extending silver  
10 strips 26 disposed, in this case, over the mesh 24.

Two or more of the assemblies 10 in Figures 2 and 3 may be mechanically supported and/or electrically connected at one or both ends and/or between the ends, for example as described with reference to Figure 4, but are shown physically spaced from each other and without support  
15 or connections for clarity.

Referring now to Figure 4, two optional methods of mechanically and electrically connecting adjacent assemblies 10 in bundles each comprising three rows of three assemblies are shown in Figures 4a and b, respectively. In Figure 4a, the assemblies 10 in each row are shown  
20 connected in parallel, while in Figure 4b the assemblies 10 in each column are shown connected in parallel. In both arrangements, the connectors are formed of silver welded to the interrupted silver strips 26 of Figure 3a, but in Figure 4a they are illustrated as intermittent solid blocks 27 to provide a mechanically rigid link while in Figure 4b they are illustrated as intermittent hollow and flexible connectors 28 to better tolerate variations in shape and size of the assemblies 10.  
25 It will be appreciated that either type of connector 27 and 28 may be used to connect the rows and/or columns of tubular fuel cell assemblies and that the assemblies 10 may also be connected at one or both ends.

The solid blocks 27 or hollow connectors 28 may additionally or only connect adjacent fuel cells  
30 in each fuel cell assembly 10 in Figure 3a in series, but in Figure 4 each cell in each tubular assembly 10 is connected not to the adjacent cell on the same assembly 10, but to the nearest

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neighbour in the next column or row of tubular assemblies 10, ie. only in parallel.

### Examples

- 5 The following examples illustrate, without limiting the invention, different processes for extruding an anode layer cermet comprising NiO/10 mol% yttria-zirconia (10YSZ) on to the outside surface of an expanded Ni-mesh current collector tube such that the current collector tube is partly embedded in the extruded anode layer in order to reinforce the dried, porous anode layer. The examples also illustrate the formation of a 10YSZ electrolyte layer on the anode  
10 layer, but do not illustrate the formation of a porous cathode layer on the electrolyte layer or of a cathode-side current collector on the cathode layer. The formation of the cathode layer and cathode-side current collector may be substantially as already described.

#### Example 1:

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This example uses an organic solvent based system for extrusion of NiO/10YSZ onto a Ni mesh tube and subsequent application of a 10YSZ electrolyte layer to the outside by coating.

- A tube formed from expanded Ni mesh (5mm diameter) was pre-oxidised by heat-treatment in  
20 air at 400°C for 1 hour. An extrusion mixture was made by combining NiO and 10YSZ powders with binder, plasticiser and solvent. The NiO had a nominal particle size of 1µm with a range of 0.6 - 10µm. The 10YSZ had a nominal size of 1µm with a size range of 0.6 – 4.0µm. The ratio of NiO to 10YSZ powders was chosen to achieve a 50vol% Ni-10YSZ cermet. The powders were milled together with the binder and plasticiser in a high-shear mixer to produce  
25 a paste having a dough-like consistency.

- The paste consisted of (by weight) 81% NiO/10YSZ powder, 11% polyvinyl butiral (PVB) binder and 8% benzyl butyl phthalate (BBP) plasticiser which was mixed with solvent at a solids to solvent ratio of about 9:1 by weight. The solvent was one third by weight methyl ethyl ketone  
30 and two thirds toluene. The formulation may be varied as required in the range 77-84 weight % powder, 8-14 weight % PVB and 6-9 weight % BBP and the amount of solvent adjusted to

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achieve the required dough-like consistency for extrusion.

The Ni-tube was passed through the centre of an extrusion die and a 300 micron thick layer of the paste was extruded onto the Ni tube. After drying, the extruded structure with the Ni tube partly embedded in the cermet layer was sintered at 1400°C. A 15 micron thick 10YSZ electrolyte layer was then deposited by slurry coating onto the 2-layer structure and sintered at 1400°C.

The 10YSZ slip used for the slurry coating was prepared in the same manner as the NiO/10YSZ paste, using the same proportions of PVB binder and BBP plasticiser to the weight of powder. However in order to produce a lower viscosity in the slip, compared to the paste, the solids to solvent ratio was reduced to about 7:3, the exact proportion being adjusted to achieve the required rheology characteristics.

#### Example 2:

This example used a water based system for extrusion of NiO/10YSZ onto a Ni mesh tube and subsequent application of a 10YSZ electrolyte layer to the outside by coating.

A tube formed from expanded Ni mesh (5mm diameter) was pre-oxidised as for Example 1 above. An extrusion mixture was made by combining the NiO and 10YSZ powders described in Example 1 with binder, plasticiser and water. The ratio of NiO to 10YSZ powders was chosen to achieve a 50vol% Ni-10YSZ cermet. The powders were milled together with the binder and plasticiser in a high-shear mixer to produce a paste having a dough-like consistency.

The paste consisted of (by weight) 87% NiO/10YSZ powder, 9% polyvinyl alcohol (PVA) binder and 4% glycerol plasticiser which was mixed with water at a solids to water ratio of about 9:1 by weight. The formulation may be varied as required in the range 83-90 weight % powder, 6-12 weight% PVA and 3-6 weight % glycerol and the amount of water adjusted to achieve the required dough-like consistency for extrusion.

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The Ni-tube was passed through the center of an extrusion die and a 300 micron thick layer of the paste was extruded onto the Ni tube. After drying, the extruded structure with the Ni tube partly embedded in the cermet layer was sintered at 1400°C. A 15 micron thick 10YSZ electrolyte layer was deposited by slurry coating onto the 2-layer structure and sintered at 1400°C.

The 10YSZ slip used for the slurry coating was prepared in the same manner as the NiO/10YSZ paste, using the same proportions of PVA binder and glycerol plasticiser to the weight of powder. However in order to produce a lower viscosity in the slip, compared to the paste, the solids to water ratio was reduced to about 7:3, the exact proportion being adjusted to achieve the required rheology characteristics.

#### Example 3:

This example used an organic solvent based system for co-extrusion of a NiO/10YSZ layer and a 10YSZ layer onto a Ni mesh tube.

A tube formed from expanded Ni mesh was pre-oxidised as for Examples 1 and 2. A paste of Ni-10YSZ was prepared as described for Example 1. A paste of 10YSZ was prepared in the same manner as for the 10YSZ slip described in Example 1 except that the solids to solvent ratio was higher at about 9:1 in order to produce a paste of a dough-like consistency. The Ni-tube was passed through the centre of an extrusion die and a 300 micron thick NiO/10YSZ and a 15 micron thick 10YSZ layer were co-extruded onto the Ni tube. The obtained 3-layer structure with the Ni tube partly embedded in the cermet layer was sintered at 1400°C.

#### Example 4:

This example used a water based system for co-extrusion of a NiO/10YSZ layer and a 10YSZ layer onto a Ni mesh tube.

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A tube formed from expanded Ni mesh was pre-oxidised as for the above Examples. A paste of Ni-10YSZ was prepared as described for Example 2. A paste of 10YSZ was prepared in the same manner as for the 10YSZ slip described in Example 2 except that the solids to water ratio was higher at about 9:1 in order to produce a paste of a dough-like consistency. The Ni-tube was  
5 passed through the center of an extrusion die and a 300 micron thick NiO/10YSZ and a 15 micron thick 10YSZ layer were co-extruded onto the Ni tube. The obtained 3-layer structure with the Ni tube partly embedded in the cermet layer was sintered at 1400°C.

While the tubular fuel cells described herein are of circular cross-section, this is not essential  
10 and they may be of any suitable cross-section. The terms "tubular" and "tube" as used herein shall be construed accordingly.

Those skilled in the art will appreciate that the invention described herein is susceptible to variations and modifications other than those specifically described. It is to be understood that  
15 the invention includes all such variations and modifications which fall within its spirit and scope.

The reference to any prior art in this specification is not, and should not be taken as, an acknowledgment or any form of suggestion that that prior art forms part of the common general  
20 knowledge.

Throughout this specification and the claims which follow, unless the context requires otherwise, the word "comprise", and variations such as "comprises" and "comprising", will be understood to imply the inclusion of a stated integer or step or group of integers or steps but not  
25 the exclusion of any other integer or step or group of integers or steps.